

# Strain measurement of the directionally solidified eutectic $\text{Al}_2\text{O}_3/\text{Y}_3\text{Al}_5\text{O}_{12}$ (YAG) ceramic by neutron diffraction

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## Abstract

The eutectic  $\text{Al}_2\text{O}_3/\text{Y}_3\text{Al}_5\text{O}_{12}$  (YAG) ceramic has been reported to be composed by single-crystalline  $\text{Al}_2\text{O}_3$  and YAG, the microstructure of which is characterized by the three dimensionally entangled two single-crystalline composites. Therefore, Laue diffraction and high-resolved energy-dispersive neutron diffraction (time-of-flight method) techniques were employed to measure residual strain precisely. It was found that the YAG phase was in tension and the  $\text{Al}_2\text{O}_3$  phase was in compression with strains in the range of  $\sim 10^{-4}$  at room temperature through comparing the lattice spacings of the sintered YAG and sintered  $\text{Al}_2\text{O}_3$  as the references of strain-free materials.

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## 1. Introduction

The directionally solidified  $\text{Al}_2\text{O}_3/\text{Y}_3\text{Al}_5\text{O}_{12}$  (YAG) eutectic single composite has attracted a lot of attention because of the superior flexural strength, thermal stability and creep resistance at high temperature.<sup>1–7</sup> A most striking structural characteristic is that the  $\text{Al}_2\text{O}_3/\text{YAG}$  composite consists of two phases of single-crystal  $\text{Al}_2\text{O}_3$  and single-crystal YAG. The microstructure of this eutectic single composite observed by the scanning electron microscope (SEM) and transmission electron microscope (TEM) shows that the single-crystal  $\text{Al}_2\text{O}_3$  and single-crystal YAG were interweaved three-dimensionally with each other. Mechanical and thermal characteristics that cannot be observed in the conventional ceramics are recognized to be strongly associated with the structure of the  $\text{Al}_2\text{O}_3/\text{YAG}$  eutectic single composite. Therefore, structural information at an atomic level is very important to know the origin of the outstanding mechanical properties.

In this paper, we report a crystallographic insight, especially the residual strain, of the directionally solidified  $\text{Al}_2\text{O}_3/\text{YAG}$  eutectic single composite for elucidating the high strength mechanism. The time-of-flight (TOF) Laue method of neutron diffraction using the high resolved neutron diffractometer *Sirius*<sup>8,9</sup> will give us a lot of structural information.

## 2. Experimental

Samples used in this study are directionally solidified eutectic single  $\text{Al}_2\text{O}_3/\text{Y}_3\text{Al}_5\text{O}_{12}$  (YAG), sintered polycrystalline  $\text{Al}_2\text{O}_3$  and  $\text{Y}_3\text{Al}_5\text{O}_{12}$  (YAG). The eutectic single  $\text{Al}_2\text{O}_3/\text{YAG}$  was synthesized using the Bridgman-type equipment at the Japan Ultra-high Temperature Material Research Center. A mother ingot was obtained by preliminary melting of the mixed powders of high-purity commercial  $\alpha\text{-Al}_2\text{O}_3$  (AKP-30, Sumitomo Chemical Co. Ltd.) and  $\text{Y}_2\text{O}_3$  ( $\text{Y}_2\text{O}_3\text{-SU}$ , Shin-etsu Chemical Co. Ltd.) powders. The ingot was inserted into a Mo-crucible situated in a vacuum chamber and

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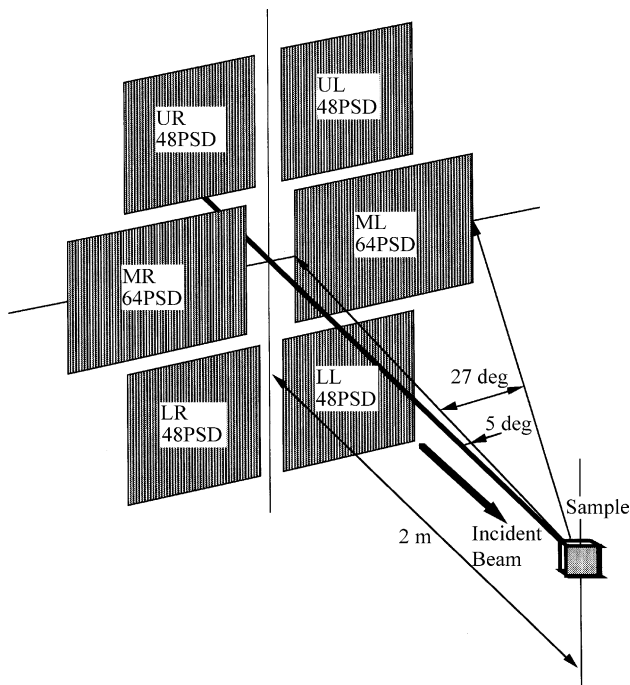


Fig. 1. Arrangement of six detector banks of *Sirius* backward bank; 64 one-dimensional position-sensitive detectors (PSDs) in the middle left (ML) and middle right (MR) banks and 48 in the lower left (LL), lower right (LR), upper left (UL) and upper right (UR) banks have been installed.

then heated by a induction heating. After sustaining the melt at 2223 K for 30 min, the Mo crucible was lower at 5 mm/h to produce the unidirectional sample. Concerning the reference samples, the mixed powders obtained by ball milling were hot pressed in a carbon die to fabricate sintered samples at 1973 K under 50 MPa for an hour in a vacuum ( $10^{-2}$  mmHg). The detailed procedure of the sample preparation has been reported elsewhere.<sup>3–7</sup> Single-crystalline and sintered samples were cut into a cube with the edge dimension of 8 mm.

Residual strain measurements of the eutectic composite  $\text{Al}_2\text{O}_3/\text{YAG}$  were carried out with TOF Laue method using the neutron diffractometer *Sirius*<sup>8,9</sup> at Neutron Science Laboratory of High Energy Accelerator Organization (KEK) in Japan. We used the backward bank of *Sirius*, in which 320 one-dimensional position-sensitive detectors (PSDs) have

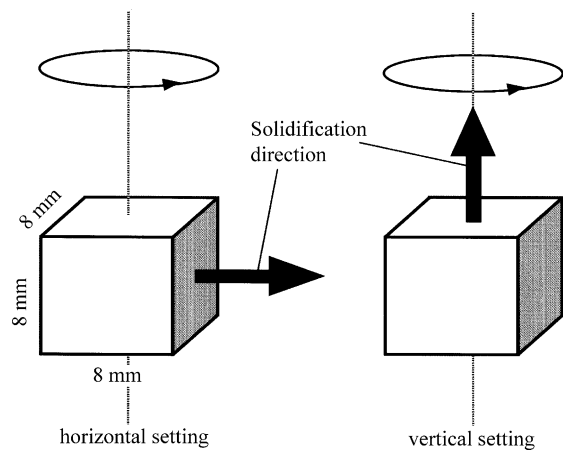


Fig. 2. Relationship between two settings and the solidification direction of the  $\text{Al}_2\text{O}_3/\text{Y}_3\text{Al}_5\text{O}_{12}$  (YAG) composite.

been installed; six detector banks for backward scattering are situated 2 m apart from the sample position as shown in Fig. 1. The scattering angle in horizontal plane is  $2\theta = 153^\circ\text{--}175^\circ$ . The number of position pixels amounts to over 80,000. The TOF diffraction pattern can be obtained over wide  $\theta$  range and wavelength ( $\lambda = 0\text{--}0.5$  nm).

The single-crystalline  $\text{Al}_2\text{O}_3/\text{YAG}$  composite was placed in the two directions at the sample position of the *Sirius* diffractometer. The solidification direction was neatly aligned horizontally or vertically toward the neutron beam direction as shown in Fig. 2. A series of TOF Laue patterns were measured for about 150 min by each  $12^\circ$  rotating around the vertical axis. Fig. 3(A) and (B) shows the TOF Laue patterns of the samples which were set horizontally and vertically. In order to estimate the precise residual strain we focused on a selected Laue spot and summed up all TOF pattern in the detector region. The residual strain was evaluated by comparison of Bragg peaks of the  $\text{Al}_2\text{O}_3/\text{YAG}$  composite with corresponding peaks of the strain-free polycrystalline  $\text{Al}_2\text{O}_3$  and YAG. The least-square curve fitting of the Bragg peaks was carried out to obtain the precise value of the lattice spacing.

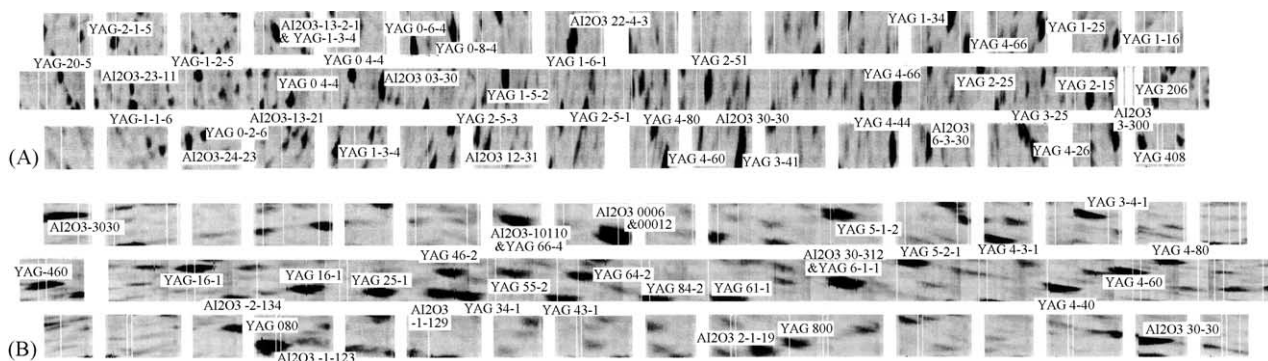


Fig. 3. Laue patterns of the horizontal setting (A) and vertical setting (B) samples toward the solidification direction for the  $\text{Al}_2\text{O}_3/\text{Y}_3\text{Al}_5\text{O}_{12}$  (YAG) composite.

The residual strain measurement with TOF Laue method is based on the Bragg's law:

$$2d \sin\theta = \lambda, \quad (1)$$

where  $\lambda$  is neutron wavelength,  $d$ , lattice spacing and  $\theta$ , scattering angle. When  $d$  changes from  $d_{hkl}^0$  to  $d_{hkl}$  elastically, the residual strain quantity  $\varepsilon_{hkl}$  is defined as follows;

$$\varepsilon_{hkl} = \frac{d_{hkl} - d_{hkl}^0}{d_{hkl}^0}, \quad (2)$$

where  $d_{hkl}^0$  is  $d$ -spacing without strain. The value of  $d_{hkl}^0$  represents a lattice spacing obtained from the strain-free polycrystalline samples.

All reflections were plotted on a Wulff net and stereographic projection to determine the reflection indices. The high-resolved TOF diffraction data obtained by *Sirius* spectrometer facilitate to index the reflections in the Laue pattern and give a precise lattice spacing of eutectic composite materials for evaluating the residual strain.

### 3. Results and discussion

Fig. 3(A) and (B) show all Laue diffraction patterns when the solidification direction of the sample was set horizontally and vertically toward the neutron beam direction. More

than 150 Laue spots were confirmed to result from single-crystalline  $\text{Al}_2\text{O}_3$  and YAG phases of the  $\text{Al}_2\text{O}_3/\text{YAG}$  composite. The reflections from  $\{116\}$ ,  $\{134\}$  and  $\{125\}$  planes of the YAG phase were observed. In other Laue spots of the YAG phase, the  $4\bar{8}0$ ,  $4\bar{6}0$ ,  $4\bar{4}0$  and  $800$  reflections belong to the  $[001]$  zone. Simultaneously, the  $\bar{3}030$  and  $30\bar{3}0$  Laue spots of the  $\text{Al}_2\text{O}_3$  phase were also observed. A Wulff net and a stereographic projection figure allow us to find that the YAG phase in the single  $\text{Al}_2\text{O}_3/\text{YAG}$  composite solidified along the direction close to  $\bar{1}\bar{1}\bar{6}$  and that the  $\text{Al}_2\text{O}_3$  phase to  $\bar{2}\bar{3}\bar{1}$  in this sample. The solidification direction observed in this work is much different with those previously reported in the papers.<sup>10,11</sup> Therefore, we can say that the solidification directions of the YAG and  $\text{Al}_2\text{O}_3$  phases in the single  $\text{Al}_2\text{O}_3/\text{YAG}$  composite depend on the solidification condition for the preparation.

The solidification direction is seen in Fig. 3(A). Laue spots near the solidification direction (left part of the figure) are sharp and isotropic. On the contrary, the Laue spots away from the solidification direction become broader. For example, the Laue spot of the  $\bar{1}\bar{2}\bar{5}$  reflection of the YAG phase is circular with  $3^\circ \times 2^\circ$ , whereas that of the  $2\bar{5}1$  reflection is oblong with  $8^\circ \times 2^\circ$ . In Fig. 3(B) where the solidification direction is vertical, all Laue spots spread out horizontally to be oblong with  $3^\circ \times 5^\circ$ – $8^\circ$ . These results suggest that when both  $\text{Al}_2\text{O}_3$  and YAG phases in the  $\text{Al}_2\text{O}_3/\text{YAG}$  composite are tangled around the solidification direction, the reflection

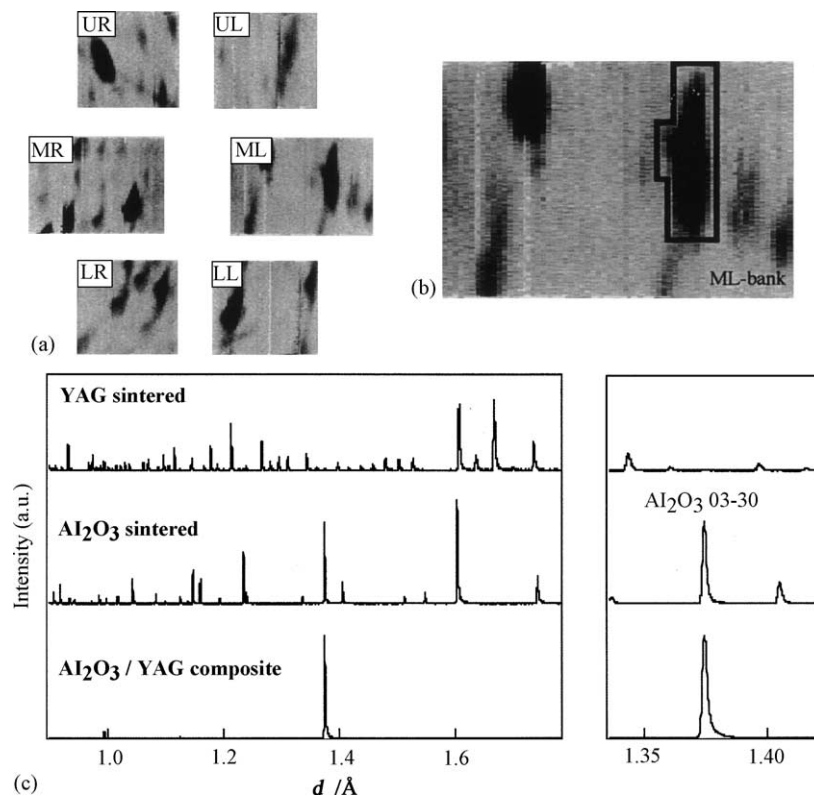


Fig. 4. Laue patterns observed by six backward detector banks: (a) and the middle left (ML) bank; (b) for the  $\text{Al}_2\text{O}_3/\text{Y}_3\text{Al}_5\text{O}_{12}$  (YAG) composite, and the TOF data from the detectors surrounded by a solid line in the middle left (ML) bank; and (c) for the sintered  $\text{Al}_2\text{O}_3$ , sintered YAG and  $\text{Al}_2\text{O}_3/\text{Y}_3\text{Al}_5\text{O}_{12}$  (YAG) composite.

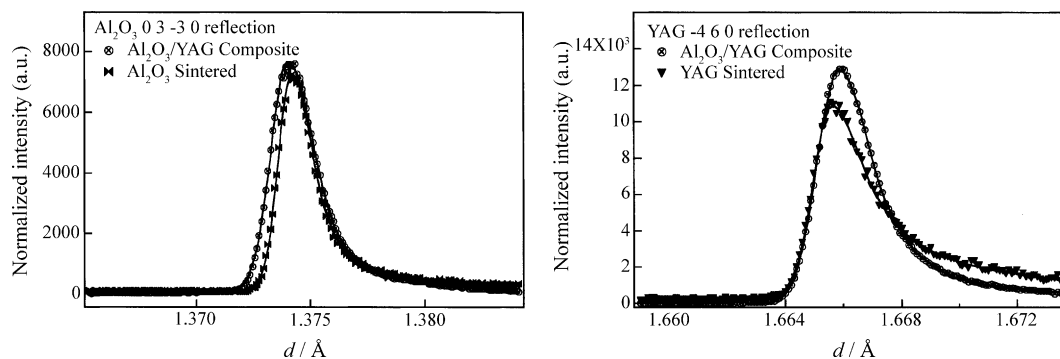


Fig. 5. Bragg peaks of  $\text{Al}_2\text{O}_3$  03  $\bar{3}$  0 and YAG  $\bar{4}$  6 0 reflections for the sintered  $\text{Al}_2\text{O}_3$ , sintered YAG and  $\text{Al}_2\text{O}_3/\text{Y}_3\text{Al}_5\text{O}_{12}$  (YAG) composite.

Table 1

The  $d$ -spacing and  $\varepsilon_{hkl}$  for the sintered  $\text{Al}_2\text{O}_3$ , sintered YAG and  $\text{Al}_2\text{O}_3/\text{Y}_3\text{Al}_5\text{O}_{12}$  (YAG) composite

Reflection index $hkl$	$d$ -spacing (nm)			$\varepsilon_{hkl}(\times 10^{-4})$
	$\text{Al}_2\text{O}_3/\text{YAG}$ composite	$\text{Al}_2\text{O}_3$ sintered	YAG sintered	
<b><math>\text{Al}_2\text{O}_3</math> phase</b>				
03 $\bar{3}$ 0	0.137403	0.137419		−1.2
$\bar{2}$ 1 3 4	0.140497	0.140519		−1.6
0006	0.216586	0.216662		−3.5
$\bar{2}$ 1 1 9	0.123468	0.123504		−2.9
30 $\bar{3}$ 1 2	0.085038	0.085069		−3.7
<b>YAG phase</b>				
0 $\bar{6}$ 4	0.166601		0.166538	3.8
$\bar{1}$ $\bar{6}$ 1	0.194898		0.194835	3.2
$\bar{2}$ $\bar{5}$ 1	0.219379		0.219284	4.3
4 $\bar{4}$ 4	0.173462		0.173394	3.9
$\bar{4}$ 6 0	0.166585		0.166562	1.4

planes located away from the solidification direction in the reciprocal space are slightly tilted from the normal position to reduce the strain which results from the unidirectional solidification of two phases.

The evaluation of the residual strain was carried out by summing up all TOF patterns (Fig. 4(c)) in the detector region from the selected Laue spot (Fig. 4(b)) in the TOF Laue diffractometry for not only the  $\text{Al}_2\text{O}_3/\text{YAG}$  composite but also the polycrystalline  $\text{Al}_2\text{O}_3$  and YAG, as shown in Fig. 4. The Bragg reflections of the polycrystalline  $\text{Al}_2\text{O}_3$  and YAG in the corresponding detector region of the  $\text{Al}_2\text{O}_3/\text{YAG}$  composite were measured as the reference values of strain-free samples indispensably to get precise residual strains. Fig. 5 shows the enlarged Bragg peaks of  $\text{Al}_2\text{O}_3$  03  $\bar{3}$  0 reflection and YAG  $\bar{4}$  6 0 reflection for the  $\text{Al}_2\text{O}_3/\text{YAG}$  composite, the polycrystalline  $\text{Al}_2\text{O}_3$  and YAG, respectively.

Some of the residual strain values  $\varepsilon_{hkl}$  are summarized in Table 1. In both phases of the  $\text{Al}_2\text{O}_3/\text{YAG}$  composite the magnitude of  $\varepsilon_{hkl}$  was the order of  $10^{-4}$  percent strain. Accordingly, it is quite small to measure appreciable residual strain within the measurement accuracy by a normal X-ray diffraction technique.<sup>11</sup> The strain value of the  $\text{Al}_2\text{O}_3/\text{YAG}$  composite is 10 times smaller than those of another composite samples.<sup>11,12</sup> Moreover, it is very important that all values of  $\varepsilon_{hkl}$  in the  $\text{Al}_2\text{O}_3$  phase were found to be negative while those in the YAG phase positive. Same results have

been reported in the previous measurement of the different sample with the dimensions of 5 mm  $\times$  5 mm  $\times$  50 mm. The order of magnitude of  $\varepsilon_{hkl}$  in the previous data<sup>10,13</sup> was also  $10^{-4}$ . The signs of the residual strain of the  $\text{Al}_2\text{O}_3$  and YAG phases indicate that the  $\text{Al}_2\text{O}_3$  phase is in the compression state and the YAG phase is in the tension state. The structural characteristics that the sign of the strain value is negative and positive for the  $\text{Al}_2\text{O}_3$  and YAG phases, respectively, and the orders are almost the same and small values of  $10^{-4}$  may represent the causes of the high strength of the eutectic single  $\text{Al}_2\text{O}_3/\text{YAG}$  composite. Accordingly, in the future we should measure the variation of the residual strain of the eutectic single  $\text{Al}_2\text{O}_3/\text{YAG}$  composite depending on the temperature to clarify the mechanism of the high temperature strength and ductility.

#### 4. Conclusions

The structural information obtained from the eutectic single  $\text{Al}_2\text{O}_3/\text{Y}_3\text{Al}_5\text{O}_{12}$  (YAG) composite leads us to get the following conclusions.

- (1) The TOF Laue method using the *Sirius* spectrometer allows us to determine the orientations of the  $\text{Al}_2\text{O}_3$  and YAG phases of the directionally solidified  $\text{Al}_2\text{O}_3/\text{YAG}$

composite. The YAG phase solidified along the direction close to  $\bar{1}\bar{1}\bar{6}$  and the  $\text{Al}_2\text{O}_3$  phase to  $\bar{2}\bar{3}\bar{1}$ , respectively.

- (2) It is inferred from the horizontal broadening observed in the vertical setting of the sample that both single-crystalline  $\text{Al}_2\text{O}_3$  and YAG phases were slightly distorted to reduce the structural strain resulted from the unidirectional solidification of the two phases.
- (3) The high resolved measurement of the structure clearly indicates that the  $\text{Al}_2\text{O}_3$  phase is in compression and the YAG phase is in tension with strains of the order of  $10^{-4}$ .

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